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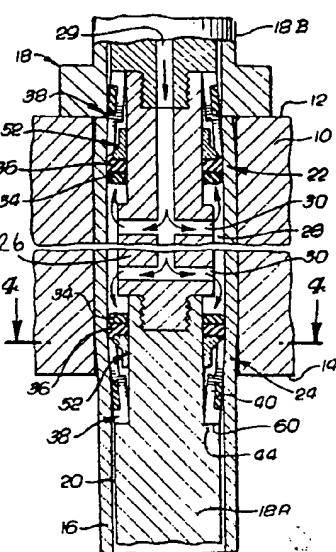
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㉒ Swaging apparatus having elastically deformable members.

㉓ A swaging apparatus includes a mandrel (18) to be inserted in a tube (16) that is to be expanded radially. A pair of seals (22, 24) define the axial boundaries of an annular pressure zone (28) between the mandrel (18) and the tube (16). Each seal includes a support (38) formed by a plurality of arcuate segments elastically held together by a ring (40) and presenting a cam surface (50). An annular cam member (52) interacts with the cam surface (50) to expand the support radially in response to swaging pressure in the pressure zone (28), thereby preventing inelastic deformation of an elastic seal member (36) on the high pressure side of the support (38).



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- 2 -

It has been found to be desirable to use two-element seals. The primary seal element, which comes into direct contact with the hydraulic fluid, is relatively soft. Usually, a rubber O-ring is used. An adjacent element, referred to as a backup member, is more rigid but still behaves elastically at the high pressures applied to it. A polyurethane ring is well suited to this use. It is compressed axially by the swaging pressure and expands radially as the tube 5 expands.

While a backup member prevents extrusion damage to the primary seal element, it has been found that at high swaging pressures the backup member itself may be inelastically deformed by extrusion into an adjacent 10 annular gap on the low pressure side of the seal that necessarily widens as the tube expands.

The present invention aims to provide an improved swaging apparatus in which the problem of destructive inelastic extrusion of the elastic element 15 or elements of the seal is minimized or eliminated.

The present invention accomplishes the above objective. It includes a swaging mandrel to be inserted axially in a tubular structure, thereby defining a pressure zone extending axially along the mandrel and the 20 surrounding structure. Preferably the mandrel defines a conduit by which pressurized hydraulic fluid can be introduced into an annular volume between the mandrel and the tube. Defining the axial boundaries of the pressure zone are a pair of seals, one or both of which 25 includes a support formed by a plurality of arcuate segments. Upon the application of a longitudinal force attributable to the swaging pressure, these segments are introduced into the annular volume between the mandrel and the tube. Defining the axial boundaries of the pressure zone are a pair of seals, one or both of which 30 includes a support formed by a plurality of arcuate segments. Upon the application of a longitudinal force attributable to the swaging pressure, these segments are spread out radially, against the inside of the tubular structure, closing off the extrusion gap between the 35 mandrel and the tubular structure. Preferably, the segments are made of a relatively inelastic material such as steel. They can be made to pivot at the end of the support farthest from the pressure zone so that the end

- 4 -

Fig 1 is a perspective view of a swaging mandrel embodying the present invention, the mandrel being depicted as inserted in a tube in a bore of a tube sheet, only a fragmentary portion of the tube sheet being shown and the tube being broken away to expose one end of the mandrel;

Fig 2 is a longitudinal cross-sectional view of the mandrel, tube and tube sheet of Fig 1, the mandrel being in position to begin swaging and a center portion of the entire structure being omitted to reduce the size of the figure;

Fig 3 is another longitudinal cross-sectional view similar to Fig 2 showing the mandrel, tube and tube sheet after swaging has taken place and while the swaging pressure is still being applied;

Fig 4 is a transverse cross-sectional view of the mandrel, tube and tube sheet taken along the line 4-4 of Fig 3;

Fig 5 is an enlargement of a fragmentary portion of the structure of Fig 2 indicated by the arrow 5; and

Fig 6 is an exploded view of various components of one seal of the mandrel.

A thick steel tube sheet 10 of the type used in heat exchangers, such as those that form part of nuclear power plants, has a plurality of bores that extend through it perpendicularly to its primary and secondary surfaces 12 and 14, respectively. A plurality of steel tubes are positioned in these bores to be expanded radially by hydraulic swaging to form leak-proof joints that prevent fluid from migrating from the secondary side 14 of the exchanger to the primary side 12. A fragmentary portion of the tube sheet 10 receiving a single tube 16 is shown in Fig 1.

A swaging mandrel 18 having an elongated generally cylindrical body 18A and a head 18B is inserted axially into the tube 16 from the primary side 12 of the tube sheet 10. As best shown in Fig 2, a small annular

- 6 -

clearance 20 increases significantly.

To prevent destructive deformation of the O-ring 34, a second elastic seal member known as the backup member 36 is provided on the low pressure side of the 5 O-ring (the side away from the pressure zone 28). The backup member 36, which is a polyurethane ring, is much harder than the O-ring 34, having an exemplary hardness of about 70 Shore D, but it will deform in a plastic manner at high pressure. The backup member 36, when 10 compressed axially by the force of the hydraulic fluid, will expand radially, maintaining contact with the tube 16. Due to the extremely high swaging pressure, the backup member 36 could be deformed inelastically and destructively into the gap between the mandrel 18 and 15 the tube 16. This extrusion gap is closed, however, by a support 38 formed by a plurality of unconnected and separate arcuate steel segments assembled side by side to make a cylinder that encircles the mandrel 18. The support 38 is first manufactured as a complete integral 20 steel cylinder which is then cut longitudinally to form the individual segments (see Fig 6).

When the segments of the support 38 are assembled about the mandrel body 18A, they are secured and urged against the mandrel by an encircling elastic 25 polyurethane band 40 that is stretched about fifty percent from its relaxed diameter. The band 40 is received by a circumferential groove 42 in the outside of the support 38 near the heel end of the support farthest from the pressure zone 28. Adjacent the heel end of the 30 support 38 is a shoulder 44 that restrains the support against axial movement along the mandrel 18 in response to swaging pressure, the mandrel being disassemblable at this point to permit the seal 24 to be installed.

At the other end of the support 38 is an undercut 35 portion 46 that defines an annular recess 48. At the mouth of the recess 48 is a conical cam surface 50 that is inclined radially outwardly and toward the pressure zone 28 forming a pointed edge 51 at the leading end

- 8 -

In the absence of the support 38, the unsupported surface of the backup member 36 would be attached to the supported area only along a circular edge and would extend uninterrupted about the entire circumference of 5 the mandrel 18 permitting an annular extrusion. In contrast, the separated, unsupported surfaces of the backup member 36 corresponding to the small gaps 62 are each attached along three of the four sides. Moreover, the maximum unsupported dimension is merely the diagonal 10 of each small area 62, which is almost insignificant when compared with the circumference of the mandrel body 18A. Thus the tendency of the backup member 36 to extrude and deform inelastically at swaging pressure can be effectively eliminated by the presence of the 15 segment support 38.

It should be noted that the small gaps 62 are each of the same size, and it would be disadvantageous if they were not since the tendency of the backup member 36 to extrude destructively is determined by the largest 20 gap presented. Uniformity of the gaps 62 is maintained because the segments of the support 38 cannot rotate about the mandrel body 18A relative to each other. They are locked in relative position because they are in tight contact with each other at the heel ends (the 25 ends away from the pressure zone 28). The location of the band 40 adjacent the heel ends produces a positive action securing the segments in their relative positions with the heels together.

The cam ring 52 tends to center the mandrel 18 within 30 the tube 16. This centering effect takes place because the ring 52 fits closely on the mandrel body 18A and cannot be cocked relative to the body because of its substantial length. It therefore forces each segment 35 of the support 38 to move radially by an equal distance, maintaining the symmetry of the support as it assumes a conical shape. The gaps 62 must therefore be of equal

-10 -

CLAIMS

1. A swaging apparatus for radially expanding a tubular structure, the apparatus comprising:

    a mandrel body to be inserted axially within the tubular structure; and

5     means for applying swaging pressure within a zone extending axially along the mandrel and including an elastically deformable member that is radially expandable against the tubular structure, characterised in that the said means further includes a plurality of 10 arcuate segments arranged to define a cylinder encircling said mandrel and cam means for spreading the segments in response to the pressure within the said zone and thereby preventing inelastic deformation of said member.

15     2. A hydraulic swaging apparatus for radially expanding a tubular structure, the apparatus comprising:

    a mandrel to be inserted axially within the tubular structure to define an annular pressure zone between the mandrel and the structure, the mandrel having a 20 conduit by which a pressurized hydraulic fluid can be introduced into the said zone; and

    a pair of axially separated seal means encircling the mandrel and thereby defining the axial boundaries of the said zone, characterised in that at least one 25 of the seal means comprises a support formed by a plurality of arcuate segments arranged to define a cylinder encircling the mandrel, at least one elastically deformable member encircling the mandrel on the high pressure side of the said support to expand radially 30 upon the application of hydraulic pressure thereto, and cam means for spreading the segments in response to the pressure within the said zone and thereby preventing inelastic deformation of the said elastically deformable member.

- 12 -

7. Apparatus according to claim 6, characterised in that the cam means is an inelastic ring formed separately from the said seal member.

5 8. Apparatus according to claim 7, characterised in that the said ring has a foot extending axially along the mandrel to prevent angular movement of the said ring relative to the mandrel, the segments defining an annular recess in which the foot is received.

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9. A hydraulic swaging apparatus for radially expanding a tubular structure, the apparatus comprising:

15 a mandrel to be inserted axially within the tubular structure to define an annular pressure zone between the mandrel and the structure, the mandrel having a conduit by which a pressurized hydraulic fluid can be introduced into the said zone;

20 a pair of axially separated seals encircling the mandrel and thereby defining the axial boundaries of the said zone, characterised in that at least one of the seals comprises (a) a support formed by a plurality of arcuate segments arranged to define a cylinder surrounding the mandrel, the segments defining a circumferential groove on the outer surface thereof, an undercut annular recess extending to the ends of the segments closest to said pressure zone, and a first cam surface at the mouth of the said recess, (b) an elastic band disposed within the said groove and urging the segments against the mandrel, (c) cam ring means having a foot extending along the mandrel into the said recess and a second cam surface engaging the first cam surface for spreading the segments at the ends thereof closest to the said zone, and (d) at least one elastic seal member disposed on the high pressure side 35 of the cam ring.

FIG. 1

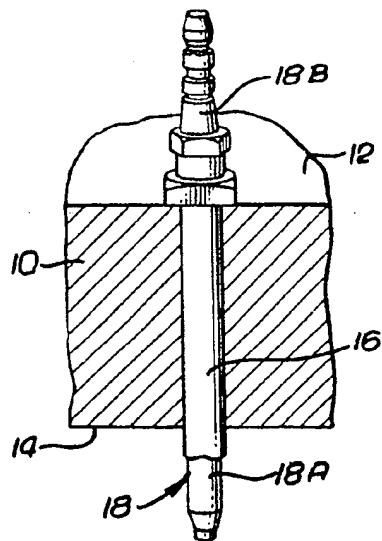


Fig. 2

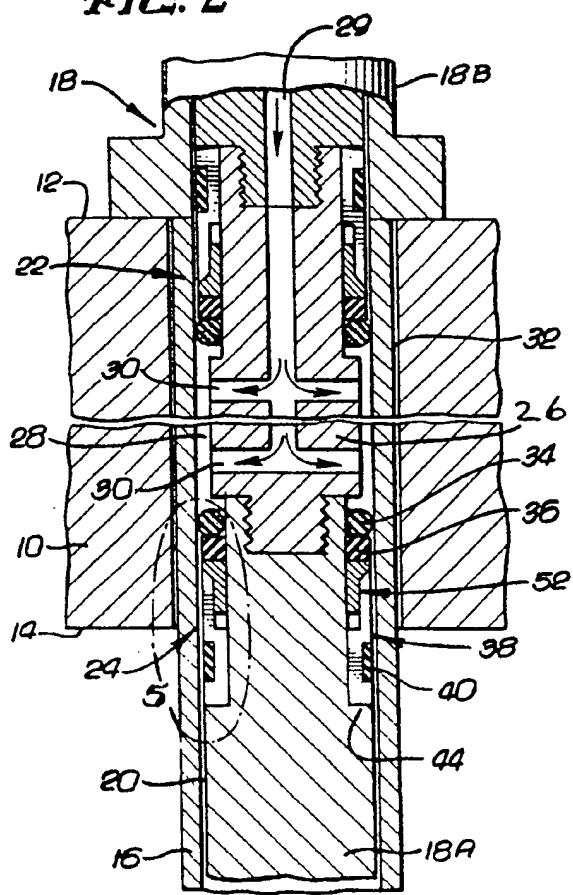
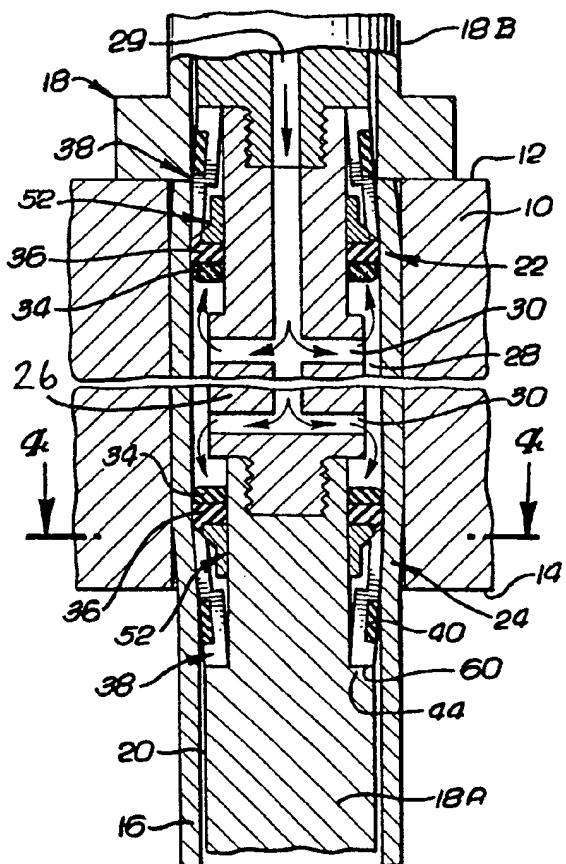


FIG. 3





European Patent  
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## EUROPEAN SEARCH REPORT

**Application number**

EP 83 30 0163

## **DOCUMENTS CONSIDERED TO BE RELEVANT**

DOCUMENTS CONSIDERED TO BE RELEVANT					
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. *)		
Y	DE-A-1 939 105 (HIGH PRESSURE COMPONENTS) * Claims 1-8 ; figure 2, references 11, 12, 15, 16 *	1	B 21 D 39/06 B 21 D 41/02		
Y	US-A-3 986 383 (PETTEYS) * Claim 1 ; figures 5, 6 *	1			
A	DE-C- 923 964 (SULZER)  * Claims 1, 2 ; figure 2 *				
			-----  TECHNICAL FIELDS SEARCHED (Int. Cl. *)  B 21 D 26/00 B 21 D 39/00 B 21 D 41/00		
The present search report has been drawn up for all claims					
Place of search	Date of completion of the search	Examiner			
BERLIN	07-03-1983	SCHLAITZ J			
CATEGORY OF CITED DOCUMENTS					
X : particularly relevant if taken alone	T : theory or principle underlying the invention				
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